

## Claims

- [c1] A method for determining a property of a flowing fluid by nuclear magnetic resonance, comprising:
  - applying a static magnetic field to the flowing fluid;
  - acquiring a suite of nuclear magnetic resonance measurements on the flowing fluid using a pulse sequence comprising a spoiling pulse, a wait time, and an acquisition pulse sequence, wherein the suite of nuclear magnetic measurements have different values for the wait time; and
  - fitting the suite of nuclear magnetic resonance measurements to a forward model for responses of the flowing fluid to derive a parameter selected from a flow speed, longitudinal relaxation times of the flowing fluid, and a combination thereof.
- [c2] The method of claim 1, wherein the acquisition pulse sequence comprises one selected from a spin-echo pulse sequence and a single pulse.
- [c3] The method of claim 1, wherein the fitting is performed by inversion of the forward model.
- [c4] The method of claim 1, further comprising estimating a

viscosity of the flowing fluid based on the derived flow speed and a pressure drop across a selected length of a pipe in which the flowing fluid travels.

- [c5] The method of claim 4, wherein the estimating is according to one selected from

$$\eta = \frac{\Delta P \cdot r_o^2}{8 \cdot \nu \cdot L} \quad \text{and} \quad \eta = K \frac{\Delta P}{\nu},$$

where  $\eta$  is the viscosity,  $\nu$  is an average speed of the flowing fluid,  $L$  is the selected length of the pipe,  $\Delta P$  is the pressure drop over the selected length of the pipe, and  $r_o$  is a radius of the pipe, and  $K$  is an experimentally determined constant.

- [c6] The method of claim 1, further comprising estimating a viscosity of the flowing fluid based on the derived longitudinal relaxation times and a gas-oil ratio of the flowing fluid.
- [c7] The method of claim 6, wherein the estimating is according to:

$$\eta_o = \frac{k \cdot T}{T_{1,LM} \cdot f(GOR)}$$

where  $\eta_o$  is the viscosity,  $k$  is an empirically determined constant for the flowing fluid,  $T$  is a temperature in Kelvin,  $T_{1,LM}$  is a logarithmic mean of the longitudinal relaxation times of the flowing fluid, and  $f(GOR)$  is an empirically determined function of the gas-oil ratio.

- [c8] A method for determining a property of a flowing fluid by nuclear magnetic resonance, comprising:
  - applying a static magnetic field to the flowing fluid;
  - acquiring a suite of nuclear magnetic resonance measurements on the flowing fluid using a pulse sequence comprising a longitudinal relaxation investigation pulse sequence and an acquisition pulse sequence, wherein the suite of nuclear magnetic measurements have different values for a delay time within the longitudinal relaxation investigation pulse; and
  - fitting the suite of nuclear magnetic resonance measurements to a forward model for responses of the flowing fluid to derive a parameter selected from a flow speed, longitudinal relaxation times of the flowing fluid, and a combination thereof.
- [c9] The method of claim 8, wherein the longitudinal-relaxation-investigation pulse comprises one selected from a inversion-recovery pulse sequence and a saturation-recovery pulse sequence.
- [c10] The method of claim 8, wherein the acquisition pulse sequence comprises one selected from a spin-echo pulse sequence and a single pulse.
- [c11] The method of claim 8, wherein the fitting is performed

by inversion of the forward model.

- [c12] The method of claim 8, further comprising estimating a viscosity of the flowing fluid based on the derived flow speed and a pressure drop across a selected length of a pipe in which the flowing fluid travels.
- [c13] The method of claim 12, wherein the estimating is according to one selected from

$$\eta = \frac{\Delta P \cdot r_o^2}{8 \cdot \nu \cdot L} \quad \text{and} \quad \eta = K \frac{\Delta P}{\nu},$$

where  $\eta$  is the viscosity,  $\nu$  is an average speed of the flowing fluid,  $L$  is the selected length of the pipe,  $\Delta P$  is the pressure drop over the selected length of the pipe, and  $r_o$  is a radius of the pipe, and  $K$  is an experimentally determined constant.

- [c14] The method of claim 8, further comprising estimating a viscosity of the flowing fluid based on the derived longitudinal relaxation times and a gas-oil ratio of the flowing fluid.
- [c15] The method of claim 14, wherein the estimating is according to:

$$\eta_o = \frac{k T}{T_{1,LM} \cdot f(GOR)}$$

where  $\eta_o$  is the viscosity,  $k$  is an empirically determined constant for the flowing fluid,  $T$  is a temperature in Kelvin,  $T_{1,LM}$  is a logarithmic mean of the longitudinal relaxation times of the flowing fluid, and  $f(GOR)$  is an empirically determined function of the gas-oil ratio.

- [c16] A method for monitoring contamination in a flowing fluid being withdrawn into a formation fluid testing tool using nuclear magnetic resonance, comprising:  
 applying a static magnetic field to the flowing fluid;  
 acquiring a suite of nuclear magnetic resonance measurements of the flowing fluid using a pulse sequence comprising a spoiling pulse, a wait time, and an acquisition pulse sequence, wherein the suite of nuclear magnetic measurements have different values for the wait time;  
 fitting the suite of nuclear magnetic resonance measurements to a forward model for responses of the flowing fluid to derive a property of the flowing fluid; and  
 monitoring a level of contamination in the flowing fluid

based on the derived property of the flowing fluid.

- [c17] The method of claim 16, wherein the property of the flowing fluid comprises one selected from a distribution of longitudinal relaxation times, a logarithmic mean of longitudinal relaxation times, and a combination thereof.
- [c18] The method of claim 16, wherein the property of the flowing fluid is a viscosity.
- [c19] A nuclear magnetic resonance apparatus, comprising:
  - a flow pipe including a prepolarization section and an investigation section, wherein the prepolarization section is upstream of the investigation section;
  - a magnet disposed around the flow pipe for creating a static magnetic field covering the prepolarization section and the investigation section;
  - an antenna disposed around the flow pipe at the investigation section for generating an oscillating magnetic field having a magnetic dipole substantially perpendicular to a magnetic dipole of the static magnetic field, and for receiving a nuclear magnetic resonance signal; and
  - a circuitry for controlling generation of the oscillating magnetic field and reception of the nuclear magnetic resonance signal by the antenna.
- [c20] The apparatus of claim 19, wherein the circuitry includes

a program having instructions for acquiring a suite of nuclear magnetic resonance measurements of a flowing fluid using a pulse sequence comprising a spoiling pulse, a wait time, and an acquisition pulse sequence.

- [c21] The apparatus of claim 20, wherein the acquisition pulse sequence comprises one selected from a spin-echo pulse sequence and a single pulse.
- [c22] The apparatus of claim 20, wherein the program further comprises instructions for fitting the suite of nuclear magnetic resonance measurements to a forward model for responses of a flowing fluid to derive a parameter selected from a flow speed, longitudinal relaxation times of the flowing fluid, and a combination thereof.
- [c23] The apparatus of claim 22, wherein the fitting is performed by inversion of the forward model.
- [c24] The apparatus of claim 22, wherein the program further comprising instructions for estimating a viscosity of the flowing fluid based on the derived flow speed or the derived longitudinal relaxation times.